

Typical Characteristics $T_C = 25^\circ\text{C}$ unless otherwise noted

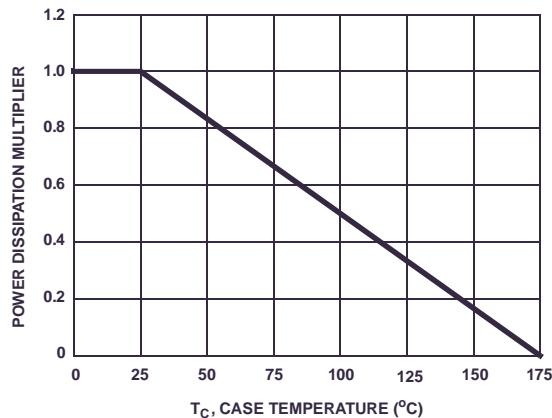


Figure 1. Normalized Power Dissipation vs Ambient Temperature

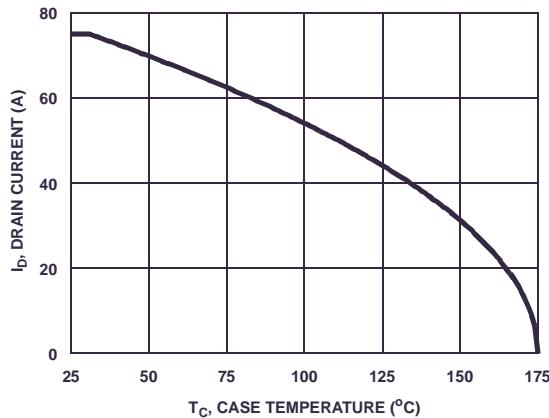


Figure 2. Maximum Continuous Drain Current vs Case Temperature

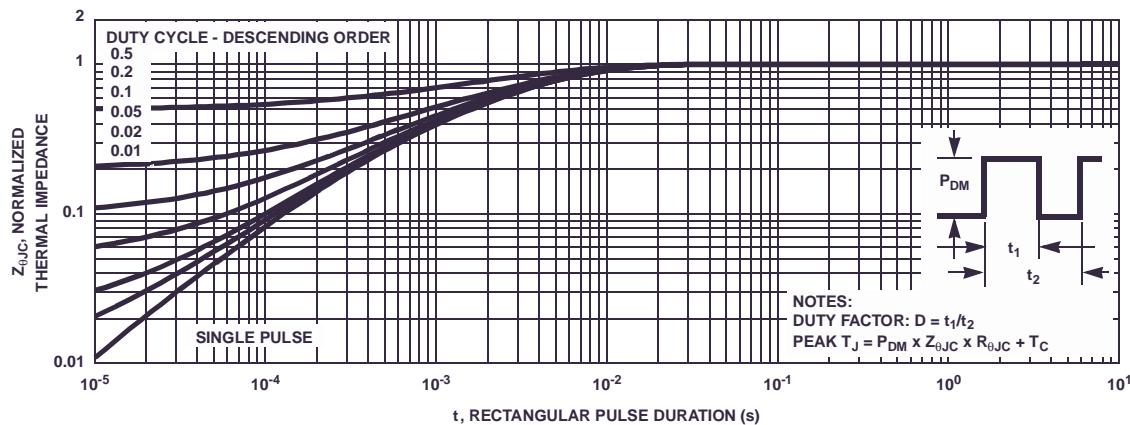


Figure 3. Normalized Maximum Transient Thermal Impedance

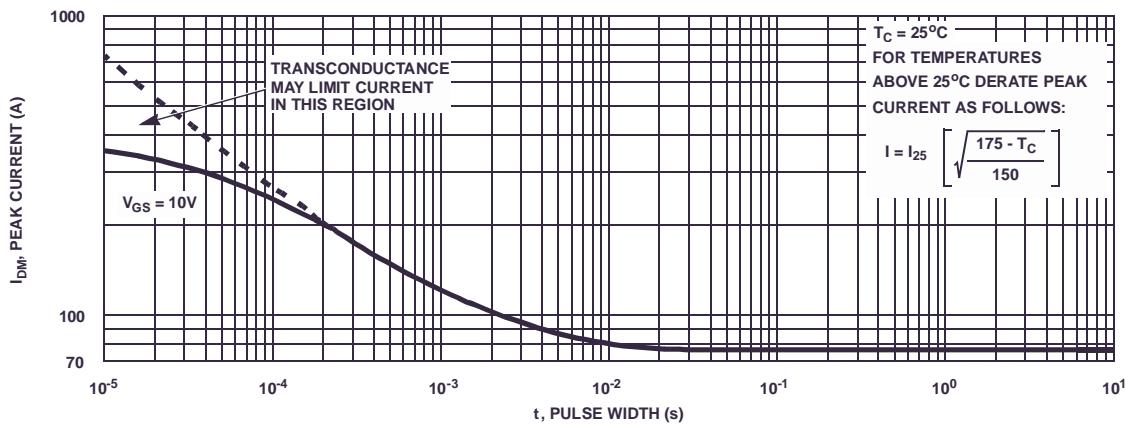
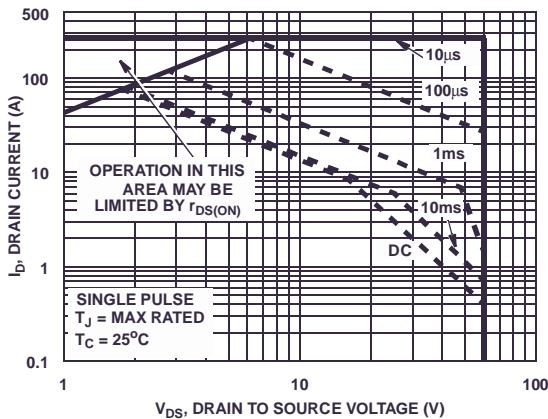
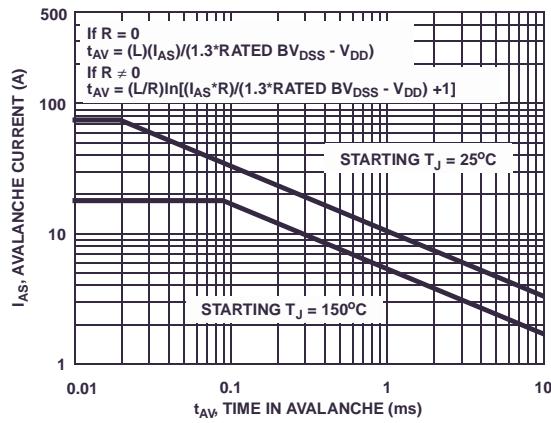
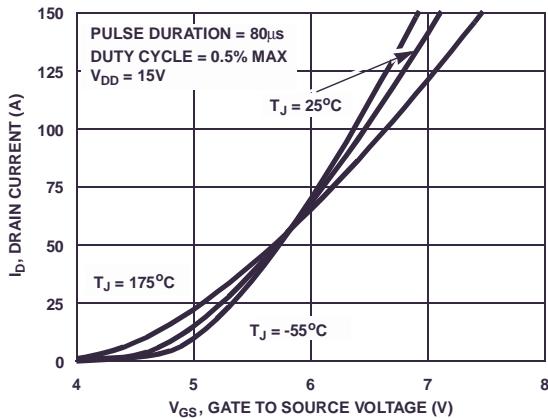
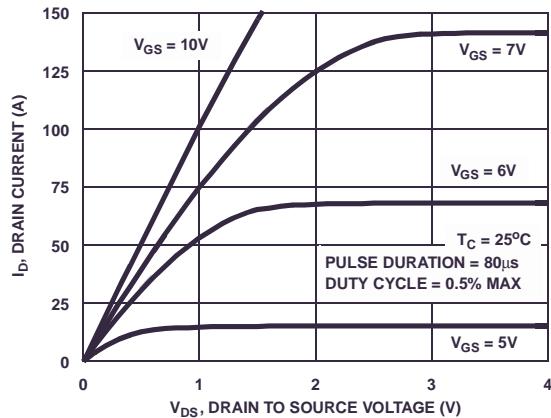
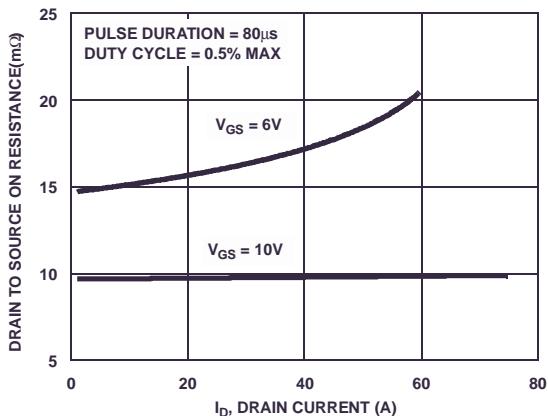
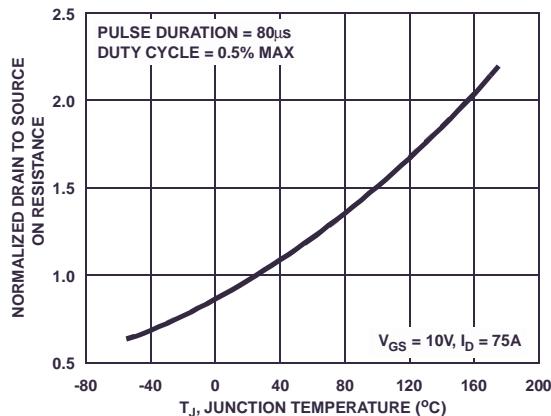


Figure 4. Peak Current Capability

Typical Characteristics $T_C = 25^\circ\text{C}$ unless otherwise noted

Figure 5. Forward Bias Safe Operating Area


NOTE: Refer to Fairchild Application Notes AN7514 and AN7515

Figure 6. Unclamped Inductive Switching Capability

Figure 7. Transfer Characteristics

Figure 8. Saturation Characteristics

Figure 9. Drain to Source On Resistance vs Drain Current

Figure 10. Normalized Drain to Source On Resistance vs Junction Temperature

Typical Characteristics $T_C = 25^\circ\text{C}$ unless otherwise noted

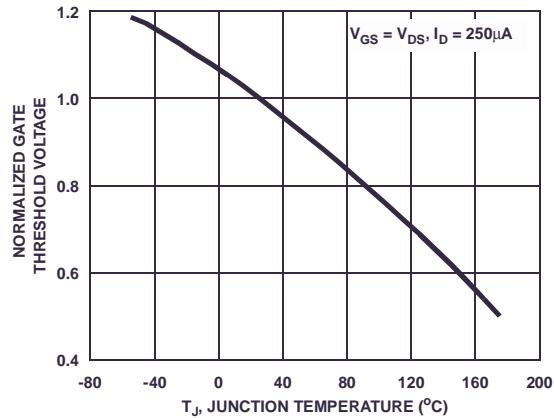


Figure 11. Normalized Gate Threshold Voltage vs Junction Temperature

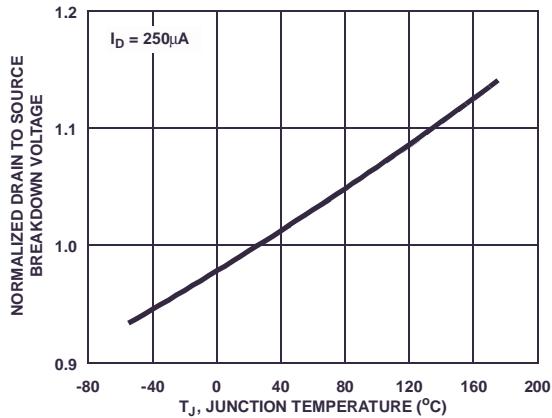


Figure 12. Normalized Drain to Source Breakdown Voltage vs Junction Temperature

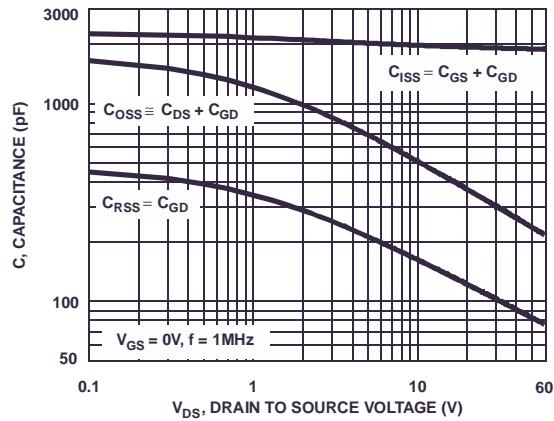


Figure 13. Capacitance vs Drain to Source Voltage

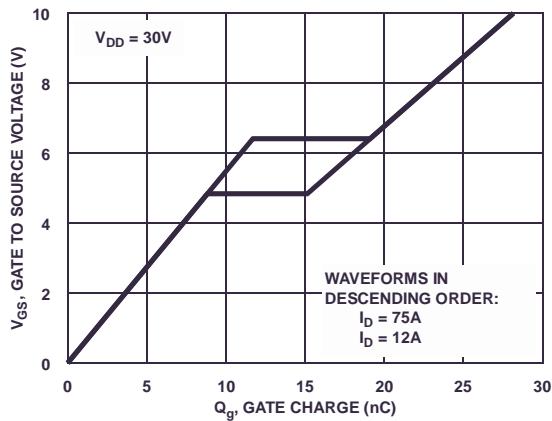


Figure 14. Gate Charge Waveforms for Constant Gate Currents

Test Circuits and Waveforms

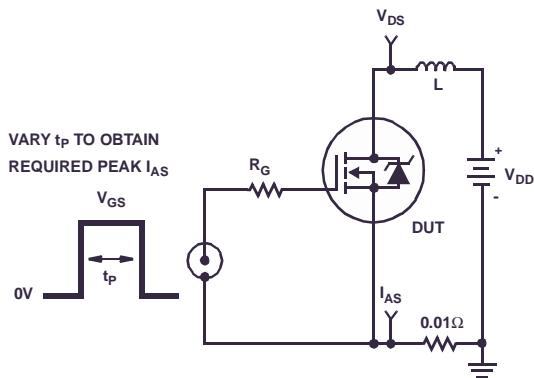


Figure 15. Unclamped Energy Test Circuit

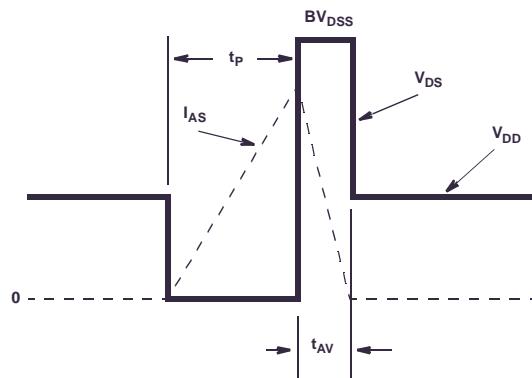


Figure 16. Unclamped Energy Waveforms

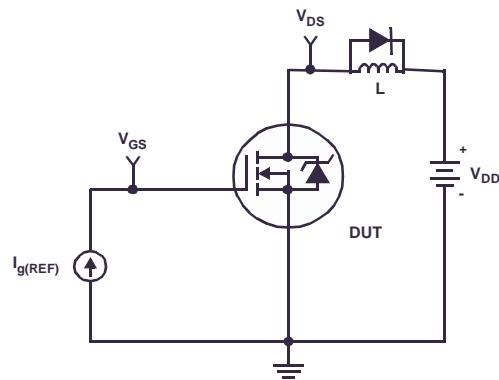


Figure 17. Gate Charge Test Circuit

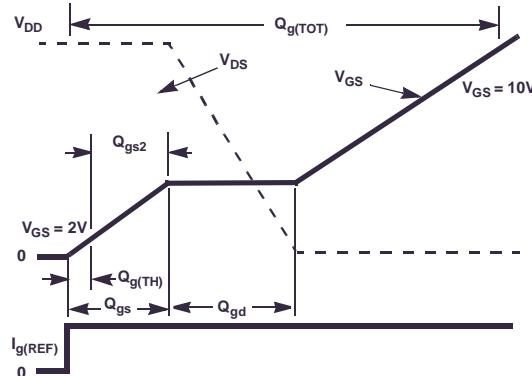


Figure 18. Gate Charge Waveforms

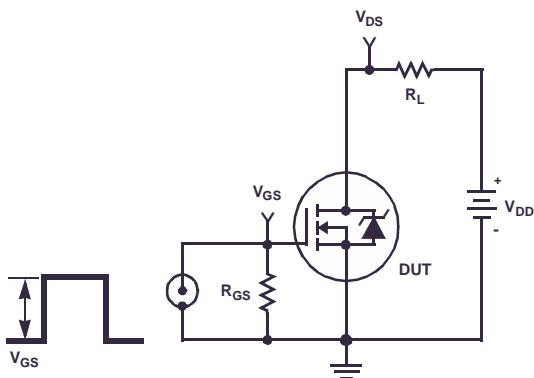


Figure 19. Switching Time Test Circuit

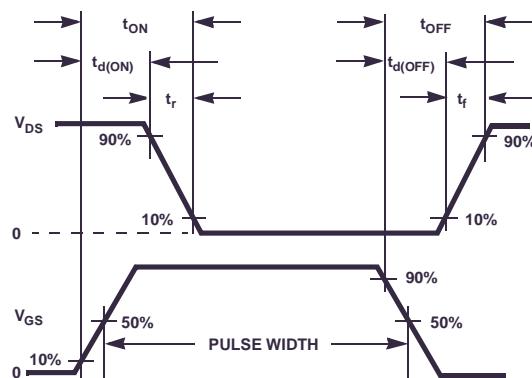


Figure 20. Switching Time Waveforms

Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A ($^{\circ}\text{C}$), and thermal resistance $R_{\theta JA}$ ($^{\circ}\text{C}/\text{W}$) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \quad (\text{EQ. 1})$$

In using surface mount devices such as the TO-263 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

1. Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
2. The number of copper layers and the thickness of the board.
3. The use of external heat sinks.
4. The use of thermal vias.
5. Air flow and board orientation.
6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the $R_{\theta JA}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\theta JA} = 26.51 + \frac{19.84}{(0.262 + \text{Area})} \quad (\text{EQ. 2})$$

Area in Inches Squared

$$R_{\theta JA} = 26.51 + \frac{128}{(1.69 + \text{Area})} \quad (\text{EQ. 3})$$

Area in Centimeters Squared

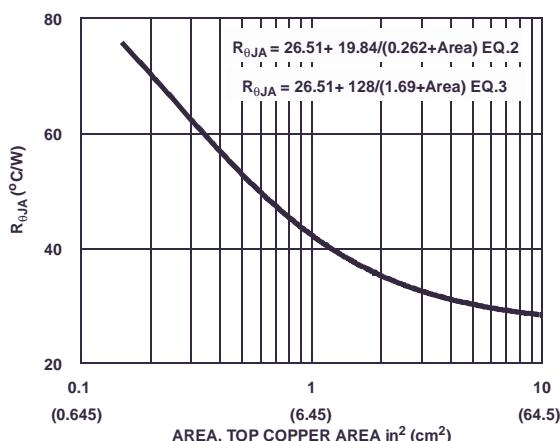
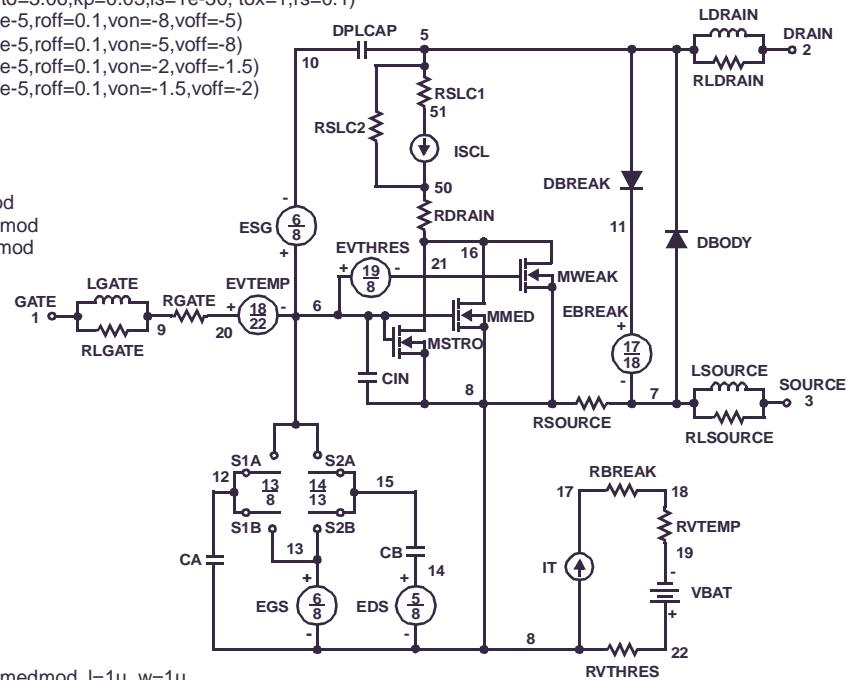


Figure 21. Thermal Resistance vs Mounting Pad Area

SABER Electrical Model

REV July 2002
 template FDP10AN06A0 n2,n1,n3
 electrical n2,n1,n3
 {
 var i iscl
 dp..model dbodymod = (isl=9e-12, nl=1.06, rs=2.7e-3, trs1=2.4e-3, trs2=1.1e-6, cjo=1.25e-9, m=5.3e-1, tt=4e-9, xti=3.9)
 dp..model dbreakmod = (rs=2.7e-1, trs1=1e-3, trs2=-8.9e-6)
 dp..model dplcapmod = (cjo=4.7e-10, isl=10e-30, nl=10, m=0.44)
 m..model mmmedmod = (type=_n, vto=-3.6, kp=5.5, is=1e-30, tox=1)
 m..model mstrongmod = (type=_n, vto=-3.6, kp=80, is=1e-30, tox=1)
 m..model mweakmod = (type=_n, vto=-3.06, kp=0.03, is=1e-30, tox=1, rs=0.1)
 sw_vcsp..model s1amod = (ron=1e-5, roff=0.1, von=-8, voff=-5)
 sw_vcsp..model s1bmod = (ron=1e-5, roff=0.1, von=-5, voff=-8)
 sw_vcsp..model s2amod = (ron=1e-5, roff=0.1, von=-2, voff=-1.5)
 sw_vcsp..model s2bmod = (ron=1e-5, roff=0.1, von=-1.5, voff=-2)
 c.ca n12 n8 = 7e-10
 c.cb n15 n14 = 7e-10
 c.cin n6 n8 = 1.8e-9
 dp.dbody n7 n5 = model=dbodymod
 dp.dbreak n5 n11 = model=dbreakmod
 dp.dplcap n10 n5 = model=dplcapmod
 spe.ebreak n11 n7 n17 n18 = 68.4
 spe.eds n14 n8 n5 n8 = 1
 spe.egs n13 n8 n6 n8 = 1
 spe.esg n6 n10 n6 n8 = 1
 spe.evthres n6 n21 n19 n8 = 1
 spe.evtemp n20 n6 n18 n22 = 1
 i.it n8 n17 = 1
 I.igate n1 n9 = 7e-9
 I.ldrain n2 n5 = 1.0e-9
 I.lsourc n3 n7 = 3e-9
 res.rlgate n1 n9 = 70
 res.rldrain n2 n5 = 10
 res.rlsourc n3 n7 = 30
 m.mmed n16 n6 n8 n8 = model=mmmedmod, l=1u, w=1u
 m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u
 m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u
 res.rbreak n17 n18 = 1, tc1=9e-4, tc2=5e-7
 res.rdrain n50 n16 = 1.6e-3, tc1=2.5e-2, tc2=7.8e-5
 res.rgate n9 n20 = 3.6
 res.rslc1 n5 n51 = 1e-6, tc1=1e-3, tc2=3.5e-5
 res.rslc2 n5 n50 = 1e-3
 res.rsource n8 n7 = 6e-3, tc1=1e-3, tc2=1e-6
 res.rvthres n22 n8 = 1, tc1=-5.9e-3, tc2=-1.3e-5
 res.rvttemp n18 n19 = 1, tc1=-2.3e-3, tc2=1.3e-6
 sw_vcsp.s1a n6 n12 n13 n8 = model=s1amod
 sw_vcsp.s1b n13 n12 n13 n8 = model=s1bmod
 sw_vcsp.s2a n6 n15 n14 n13 = model=s2amod
 sw_vcsp.s2b n13 n15 n14 n13 = model=s2bmod
 v.vbat n22 n19 = dc=1
 equations {
 i (n51->n50) +=iscl
 iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))*((abs(v(n5,n51)*1e6/250))** 7))
}



SPICE Thermal Model

REV 23 July 2002
FDP10AN06A0T

CTHERM1 TH 6 3.2e-3
CTHERM2 6 5 3.3e-3
CTHERM3 5 4 3.4e-3
CTHERM4 4 3 3.5e-3
CTHERM5 3 2 6.4e-3
CTHERM6 2 TL 1.9e-2

RTHERM1 TH 6 5.5e-4
RTHERM2 6 5 5.0e-3
RTHERM3 5 4 4.5e-2
RTHERM4 4 3 1.5e-1
RTHERM5 3 2 3.37e-1
RTHERM6 2 TL 3.5e-1

SABER Thermal Model

SABER thermal model FDP10AN06A0T

```
template thermal_model th tl
thermal_c th, tl
{
  ctherm.ctherm1 th 6 =3.2e-3
  ctherm.ctherm2 6 5 =3.3e-3
  ctherm.ctherm3 5 4 =3.4e-3
  ctherm.ctherm4 4 3 =3.5e-3
  ctherm.ctherm5 3 2 =6.4e-3
  ctherm.ctherm6 2 tl =1.9e-2

  rtherm.rtherm1 th 6 =5.5e-4
  rtherm.rtherm2 6 5 =5.0e-3
  rtherm.rtherm3 5 4 =4.5e-2
  rtherm.rtherm4 4 3 =1.5e-1
  rtherm.rtherm5 3 2 =3.37e-1
  rtherm.rtherm6 2 tl =3.5e-1
}
```

